

The role of slags and other by-products within circular economy in the steel industry

- Carbon footprint calculation for slag from a reducing electric furnace
- Dr. Julian Suer (tkSE | CCM/SSP/Alternative Technologies)

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Slag Workshop

Carbon footprint calculation for slag from a reducing electric furnace

06.03.2025 | Dr. Julian Suer (tkSE | CCM/SSP/Alternative Technologies)



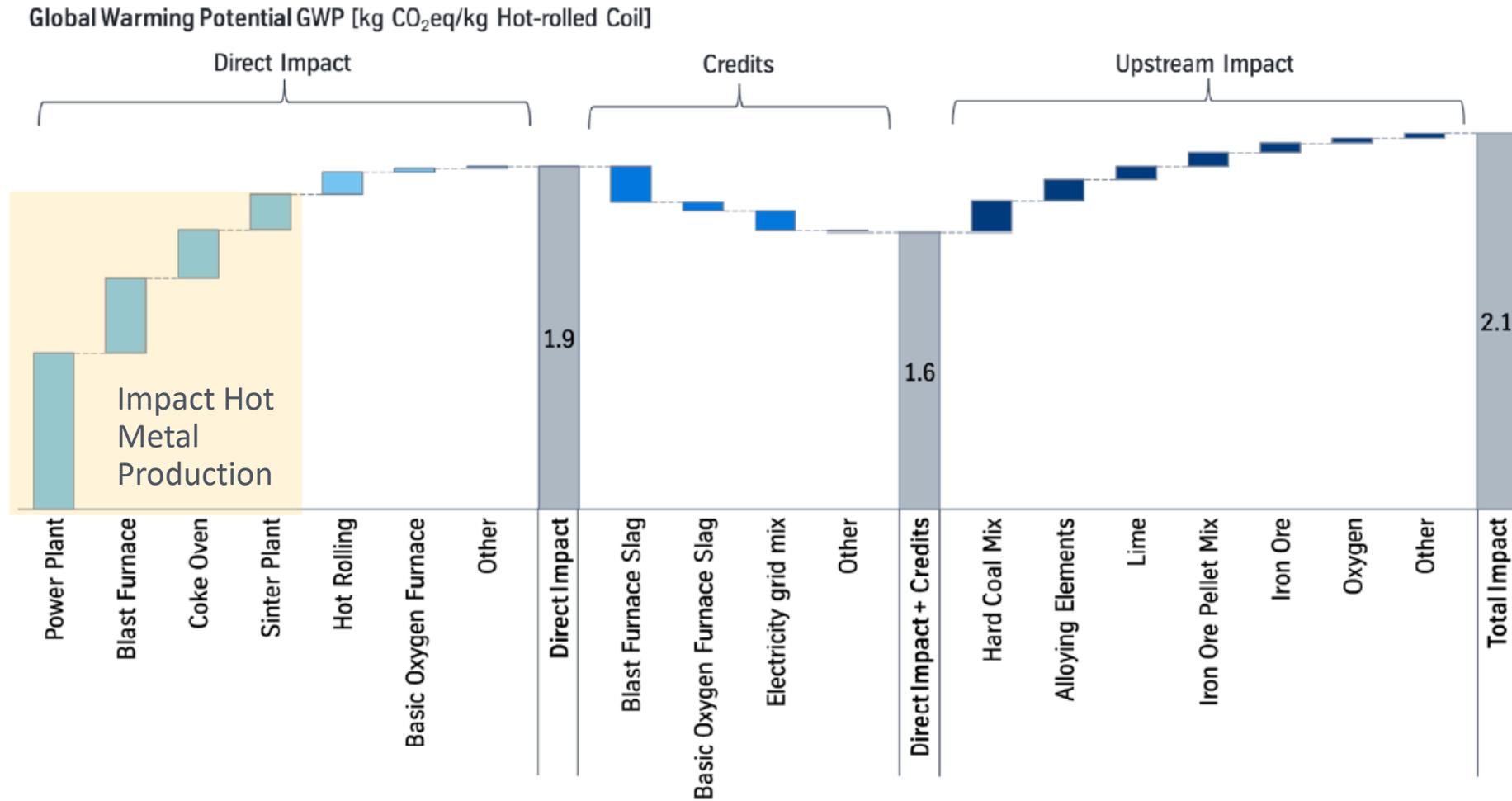
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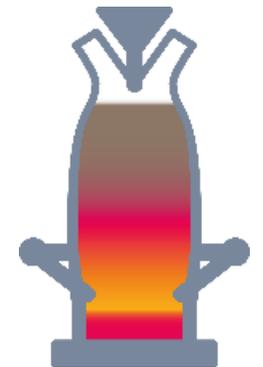
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Transformation of the steel industry

Base Case



Blast Furnace Route



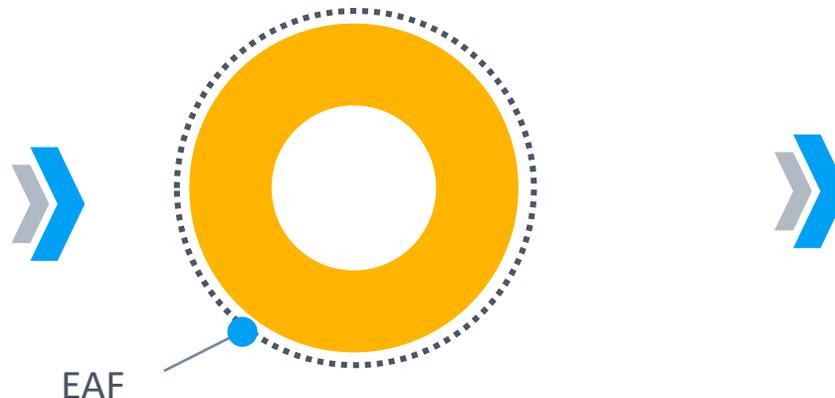
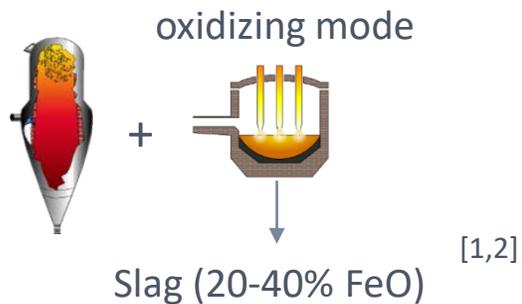
Suer, J.; Ahrenhold, F.; Traverso, M.: Carbon Footprint and Energy Transformation Analysis of Steel Produced via a Direct Reduction Plant with an Integrated Electric Melting Unit. Journal of Sustainable Metallurgy (2022). DOI:10.1007/s40831-022-00585-x



Low emission steel production routes

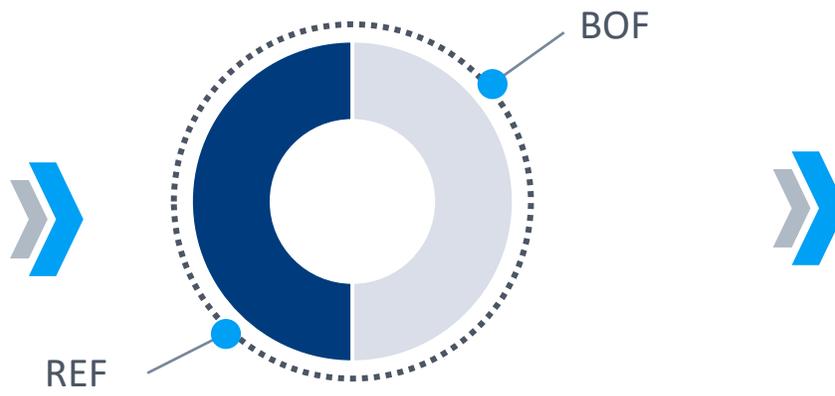
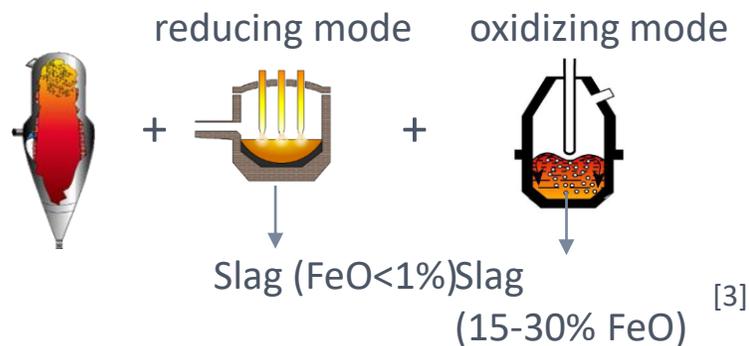
Impact on slag production

DRI-EAF – Route



Single slag work leads to low valuable slag

DR-REF-BOF – Route



Extra effort of dividing slag work on two processes allows to produce high-valuable slag in REF

Shared slag work allows to produce cement clinker substitute in REF

[1] Stagnoli, P. (2020). Decarbonising the steelmaking process. Steel Times International, 44(5), 24-27.

[2] Lüngen, I. H. B., & Schmöle, P. (2022). Wege zu einer klimaneutralen Stahlerzeugung.

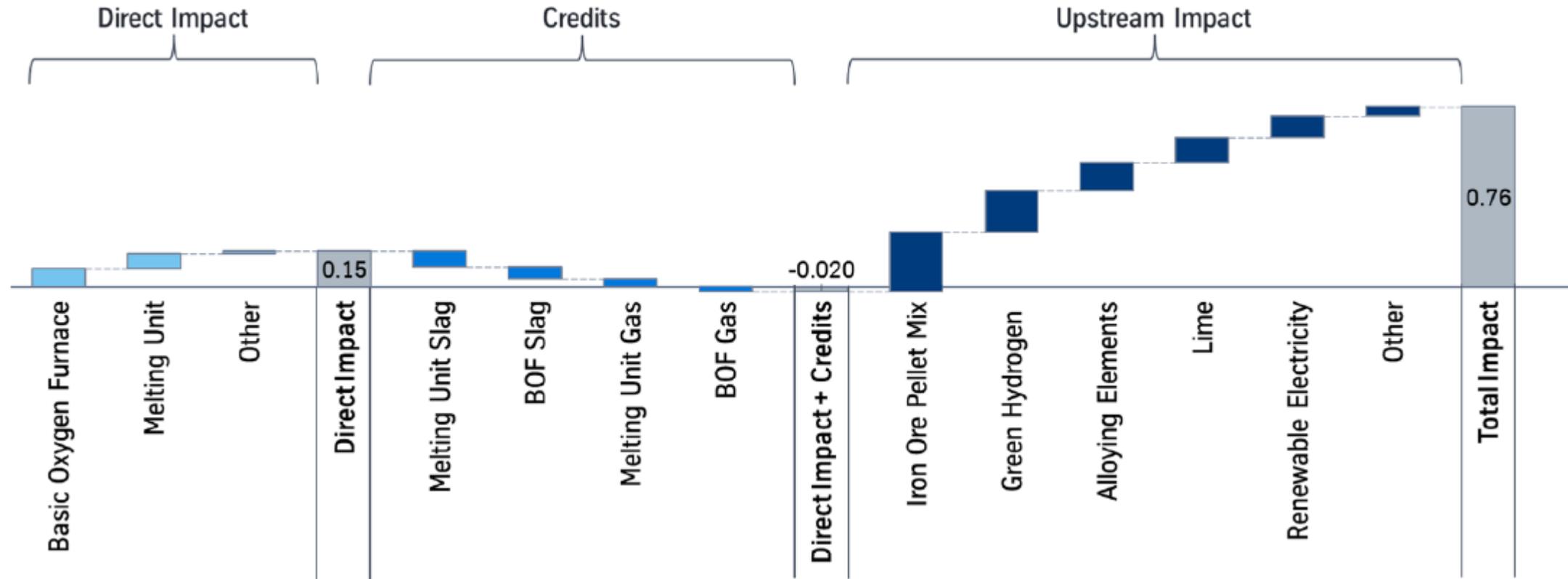
[3] Zago, Vernilli, Cascudo (2023): The reuse of basic oxygen furnace slag as concrete aggregate to achieve sustainable development: characteristics and limitations



Transformation of the steel industry

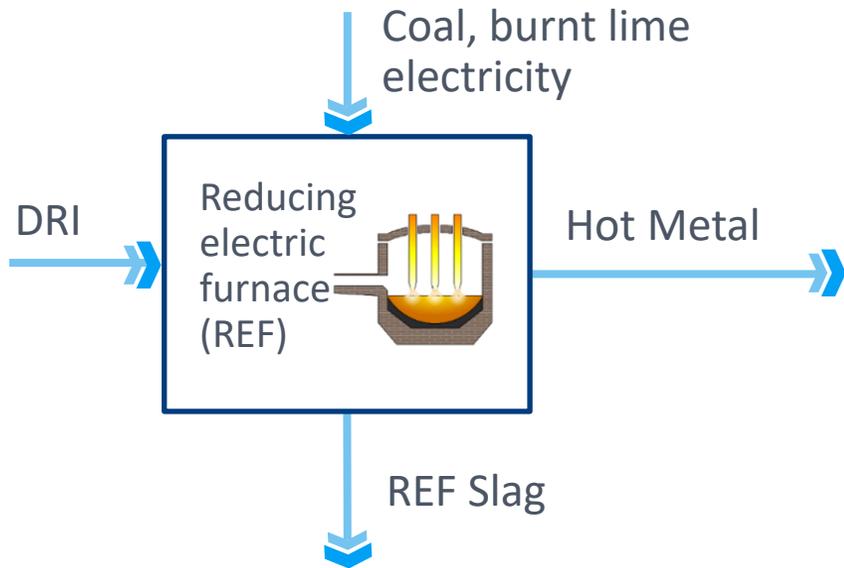
Hydrogen based DR + REF + BOF - Route

Global Warming Potential GWP [kg CO₂eq/kg Hot-rolled Coil]



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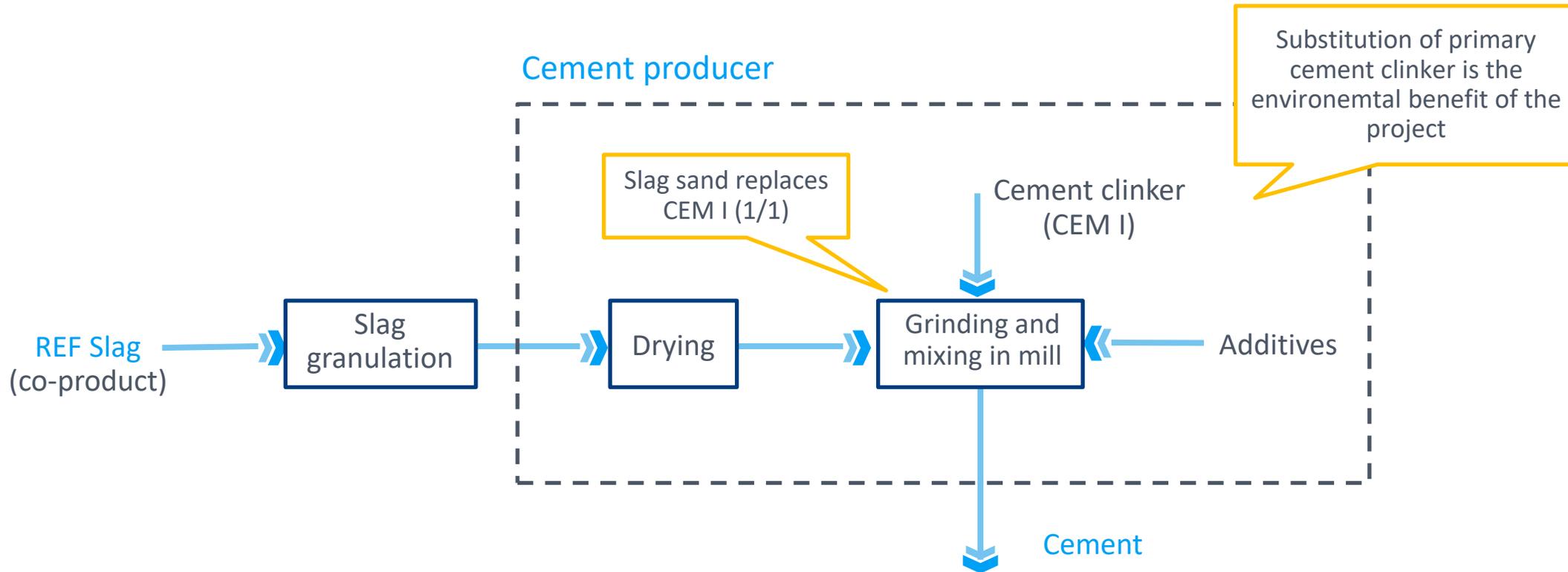


Slag Composition

$$B = \frac{CaO}{SiO_2} = 1.1$$

Element	Share [%]
SiO ₂	36
CaO	40
Al ₂ O ₃	17
FeO	0,3
MgO	5

Trials Series 2, July 2024



1 kg granulated REF slag substitutes 1 kg cement clinker (CEM I)



Cement Clinker Substitute



GWP [kg CO₂e/kg CEM I] ¹

0.84

- REF slag substitutes CEM I 1/1
- Primary cement clinker has a carbon footprint of 0.84 kg CO₂e/kg CEM I¹
- How is the benefit shared between steel and cement producer within the blast furnace route ?

[1] According to Sphera database „RER: CEM I 42.5 (burden free binders)“



Evaluation of blast furnace slag in ISO norms

LCA and EPDs for blast furnace slag

ISO 14044 (LCA)

Step 1:

Allocation should be avoided

- **System partitioning**  Separating the burden for the hot metal and for the slag production; not practical for blast furnace operation because of highly integrated processes
- **System expansion**  Expanding the product system to include additional functions related to the co-product (**Credit methodology**)

Step 2:

Apply allocation 

System expansion:
Slag value 0.84 kg CO_{2eq}/kg ²

EN 15804 (EPD)

Step 1:

Allocation should be avoided

- **System partitioning** 

Step 2:

Apply allocation:

Apply **economic allocation** 

Step 3:

If the difference in income generated by the products is small;¹ the **allocation** must be based on **physical** characteristics (mass, volume) 



Area of conflict

Economic allocation:
Slag value 0.1 kg CO_{2eq}/kg ³

Slag evaluation depends on considered regulatory

1: Contributions to income in the order of 1% or less are considered very low. A difference in company income of more than 25 % is considered large

2: Evaluation according to CEM I according to World Steel.

3: LESS Rulebook: [20240422_Annex_LESS-Rulebook.pdf](#)



Evaluation of blast furnace slag in ISO norms

LCA and EPDs for blast furnace slag

ISO 14044 (LCA)

Step 1:

Allocation should be avoided

- **System partitioning**

Separating the burden for the hot metal and for the slag production; not practical for blast furnace operation because of highly integrated processes

- **System expansion**

Expanding the product system to include additional functions related to the co-product (Credit methodology)

Step 2:

Apply allocation



System expansion:
Slag value 0.84 kg CO_{2eq}/kg²

EN 15804 (EPD)

Step 1:

Allocation should be avoided

- **System partitioning**

Step 2:

Apply allocation:

Apply **economic allocation**



Step 3:

If the difference in income generated by the products is small;¹ the allocation must be based on **physical** characteristics (mass, volume)



Might be possible for slag from a reducing electric furnace



Area of conflict

Economic allocation:
Slag value 0.1 kg CO_{2eq}/kg³

Slag evaluation depends on considered regulatory

1: Contributions to income in the order of 1% or less are considered very low. A difference in company income of more than 25 % is considered large

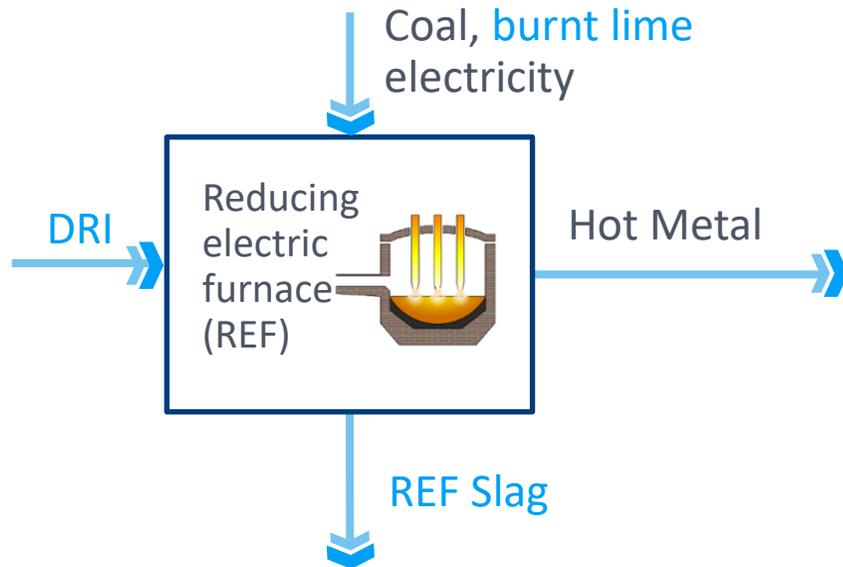
2: Evaluation according to CEM I according to World Steel.

3: LESS Rulebook: [20240422 Annex LESS-Rulebook.pdf](#)



System partitioning for reducing electric furnace

What is the burden for producing the highly reactive slag ?



Using burnt lime for:

- Viscosity
 - Desulfurization
 - Slag properties (reactivity) – extra burden for cement producer
- } required for process, anyway

Which is the amount of extra burnt lime for the slag reactivity?

A part of the used burnt lime is used for generating a highly reactive slag



Use of additional burnt lime for slag reactivity

$$\Delta = 0.14 \frac{\text{kg burnt lime}}{\text{kg Slag}} \times 1.2 \frac{\text{kg CO}_2\text{e}}{\text{kg burnt lime}}$$

$$B = \frac{\text{CaO}}{\text{SiO}_2}$$

$$B_{\text{Trials}} = 1.1$$

$$\text{SiO}_2 = 36\%$$

$$\text{CaO} = 40\%$$

$$B_{\text{min}} = 0.75^{[1]}$$

$$\text{SiO}_2 = 40\%$$

$$\text{CaO} = 30\%$$

Difference is used for slag optimization



$$0.27 \text{ kg/kg slag} < \text{CaO} < 0.40 \text{ kg/kg slag}^{[3]}$$



$$\Delta = 0.14 \frac{\text{kg burnt lime}}{\text{kg Slag}} \times 1.2 \frac{\text{kg CO}_2\text{e}}{\text{kg burnt lime}} = 0.17 \frac{\text{kg CO}_2\text{e}}{\text{kg Slag}}$$

[1] Elmomen (2017): Influence of Slag Composition and Temperature on Silicon Distribution between Slag and Hot Metal in the Egyptian Blast Furnace No.III

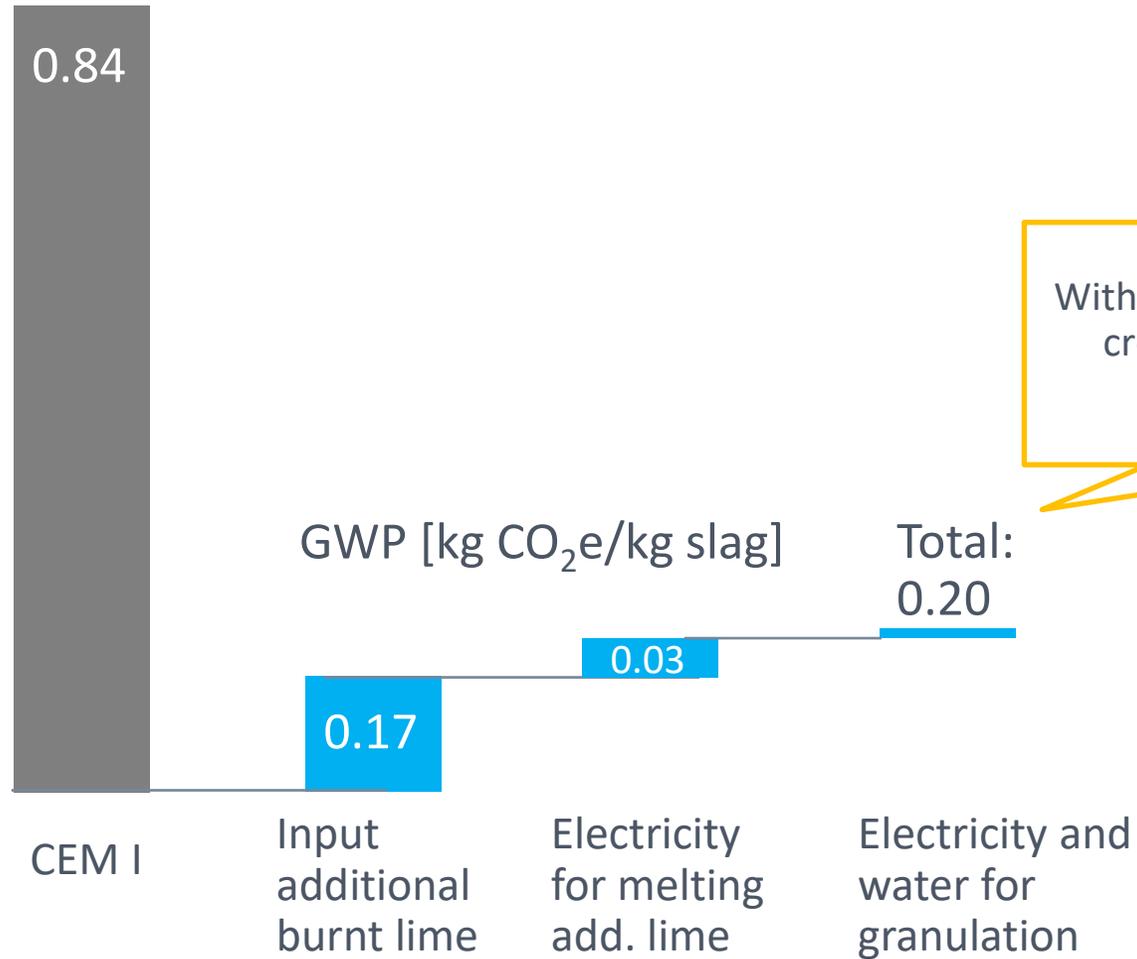
[2] Assumption. 95% CaO in burnt lime

[3] Dilution effects need to be considered



Benefit and burden of CEM I substitution

GWP [kg CO₂e/kg CEM I]



With a burden of 0.20 kg CO₂e/kg slag a cross-industriell benefit of 0.84 kg CO₂e/kg can be achieved

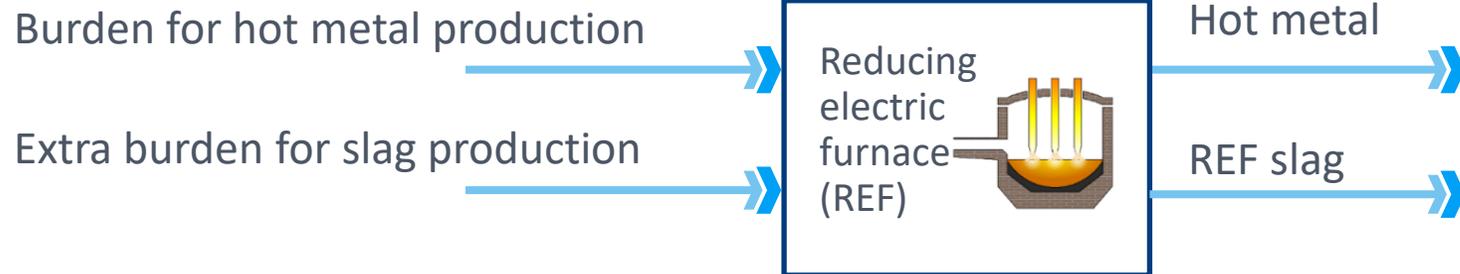


System partitioning might be possible for slag production in REF process

Simplified example for calculation of system division

- System partitioning in LCA and epds first choice
- In blast furnace route it is not practical to separate the burden for hot metal and slag production
- For a reducing electric furnace (REF) a possible methodology was presented.

System partitioning reflects the real environmental burden



Partitioning approach:

Here only the extra lime for reactive slag is considered as burden

Slag Value:

- Use of extra burnt lime for reactivity
- Melting of extra burnt lime

0.20 kg CO₂e/kg slag

Detailed engineering required:

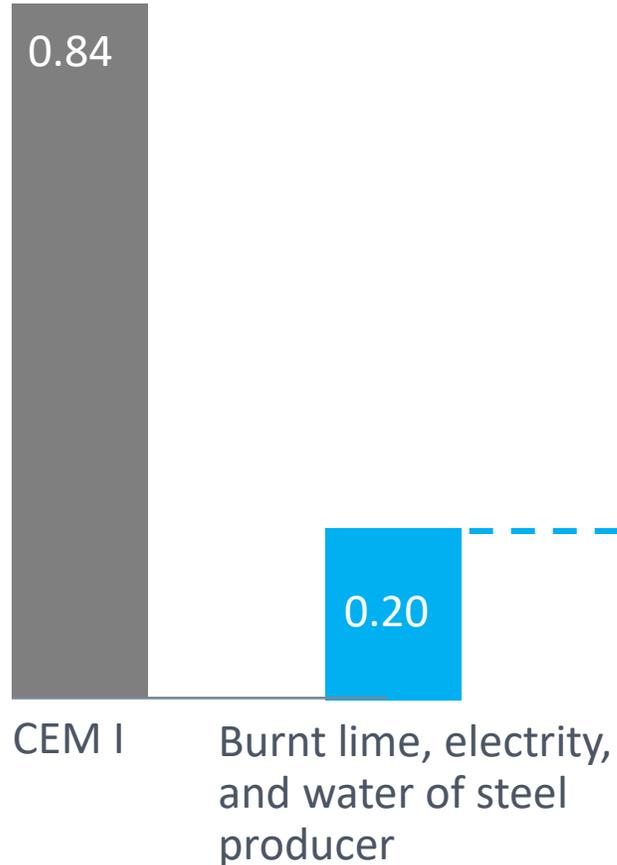
- Effects in REF are more complex than highlighted here.
- CaO content has impact on electrical conductivity; melting point etc in dependency of chemical composition needs to be evaluated
- Minimum input of burnt lime could be different from BF route because of different tapping temperatures
- More detailed calculation and primary data are necessary for system partitioning



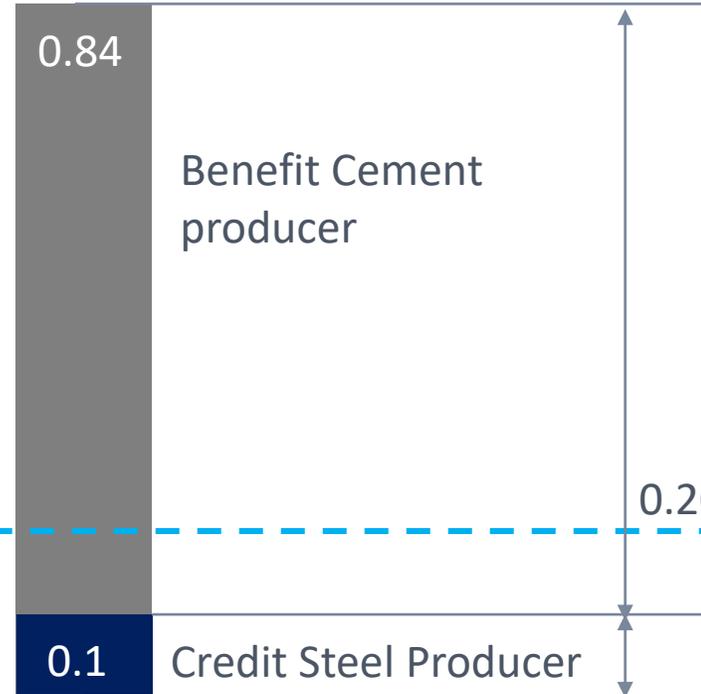
Economical allocation of slag has risk of not incentivizing steel maker



GWP [kg CO₂e/kg granulated Slag]



Economical Allocation



Total Benefit of CEM I substitution

Burden Steel Producer

0.1 kg CO₂e/kg: according to LESS approach, based on economic allocation ¹

The environmental burden of steel producer needs to be considered for giving incentive

[1] LESS Rulebook: 20240422 Annex LESS-Rulebook.pdf



- Extra effort of dividing slag work on two processes allows to produce a high valuable slag in reducing electric furnace (REF)
- Evaluation of blast furnace slag via system partitioning was not practical so far
- An example of system partitioning for the slag from the REF is presented but needs further evaluation
- 0.20 kg CO₂e/kg slag is the burden of the steel producer for the input of additional burnt lime and electricity
- With this burden a cross-industriell benefit of 0.84 kg CO₂e/kg slag can be achieved.

Thank you for your attention



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Different slag compositions

Tab. 2.5-2: Chemische Zusammensetzung von Hochofenschlacke (HO-Schl.) in M % [JUCKES, 1995].

Inhaltsstoffe	HO-Schl. in M %
SiO ₂	33-40
Al ₂ O ₃	8-14
CaO	31-42
MgO	7-15
Fe _{gesamt}	0,2-0,7
Mn _{gesamt}	0,2-0,8
P ₂ O ₅	<0,05
Na ₂ O	0,3-1,2
K ₂ O	0,6-1,2
S _{gesamt}	0,7-1,6
TiO ₂	0,1-2,7
CaO/SiO ₂	0,8-1,2
(CaO+MgO)/SiO ₂	1,0-1,3

